

GATE -AE ENGINEERING MECHANICS



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Engineering Mechanics

Chapter 1: STATICS (REST)

Newton 1st law (NFL)

 \vec{a} = Acceleration vector

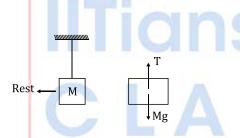
For a Particle:

 $\sum \vec{F} = 0$, then $\vec{a} = 0 \rightarrow \text{Rest}$; Uniform velocity

For a Rigid Body:

$$\Sigma \vec{F}_{ext} = 0$$
 then $\vec{a}_{cm} = 0$

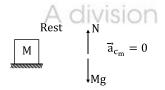
Case 1:



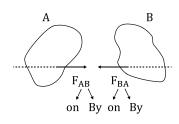
$$\vec{a}_{c_m} = 0$$
; $\sum \vec{F}_{ext} = 0$; $T - mg = 0$, $T = mg$

Exclusive GATE COACH

Case 2:

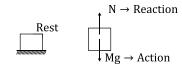


Newton's Third Law (NTL):



$$\vec{F}_{AB} = -\vec{F}_{BA}$$

Case:



Equilibrium:

Rest or uniform linear velocity

i.e.
$$\sum \vec{F} = 0$$

For Particle $\sum \vec{F} = 0$

For a rigid body $\sum \vec{F} = 0 \Rightarrow \sum \vec{F}_x = 0, \sum F_y = 0$

$$\sum \vec{F}_z = 0$$

 $\sum M = 0$ (about any point or line in plane)

System of Equilibrium:

1. Two force system

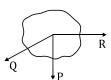
$$\vec{P} + \vec{Q} = 0, \vec{P} = -\vec{Q}$$

$$\overrightarrow{M} = 0 \rightarrow Collinear$$



2. Three Force System

For equilibrium three forces must be coplanar and con-current.



$$\vec{P} + \vec{Q} + \vec{R} = 0$$

$$\sum \overrightarrow{M} = 0$$
 (Concurrent)



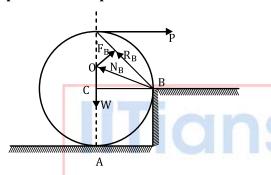
Lami's Theorem:

For a three-force system

$$Q \longrightarrow \beta$$

$$\frac{P}{\sin \alpha} = \frac{Q}{\sin \beta} = \frac{R}{\sin y}$$

Important concepts:



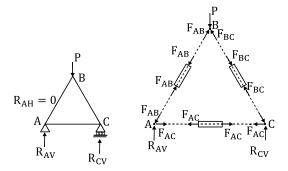
- a. As roller is about to move out of curb, normal reaction at A becomes zero, as it loses its contact at point A and cylinder or roller will be under equilibrium at verge of motion.
- b. Here comes a contact force (Resultant of normal reaction and friction at B (i.e., $R_{\rm B}$)
- c. So, only three forces are P, W, R_B which maintain equilibrium, so these must be coplanar and concurrent.
- d. If the horizontal force 'P' is applied at centre, no friction will be there i.e., reaction force at B will acts as normal reaction.

For P to be minimum its line of action should be $\bot^{\mathbf{r}}$ to R_B

Chapter 2: PLANE TRUSS

Numbers of members = m

Number of Joints = J



J = No. of Joints (Whether it is binary or ternary joint)

For perfect truss: m = 2j - 3 (D0F = 0) m < 2j - 3 Unstable truss (D0F > 0) m > 2j - 3 Redundant, stable and (D0F < 0)

indeterminate truss

Method of Joint:

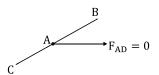
Equilibrium of joint is considered in method of joint to find loading in the member.

Procedure: Center

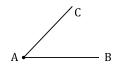
- 1. Find support reactions if required
- 2. Consider equilibrium of joint where only two members are meeting and use $\sum f_x = 0$, $\sum f_y = 0$.

Note:

At a joint if 3 members are meeting and
 members are collinear the forces in 3rd
 member = 0



2. If at a joint two members are meeting and they are non-collinear then forces in both members will be zero.



$$F_{AB} = F_{AC} = 0$$

Method of Section:

Equilibrium of a section of truss is considered.

Procedure:

- 1. Find reactions at support if required
- 2. Cut the member under consideration by section 1 1 and consider the equilibrium of either LHS at RHS of section 1 1 and use $\sum f_x = 0, \sum f_y = 0, \sum M = 0$ to find unknowns.

Note: Don't cut more than 3 members.

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Chapter 3: Principle of Virtual Work (POVW)

 $WD(Work done) = \vec{F} \cdot \vec{d}_s$

 $\vec{d}_s = \text{Displacement vector of a point where } \vec{F}$ is acting.

Principle of virtual work stats that if the system is in equilibrium then sum of virtual work by all the forces = 0

Virtual work = $F \cdot ds$

F = Actual force

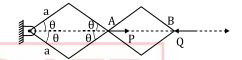
ds = virtual displacement.

Procedure:

- 1. Take any fixed point is problem as origin. fix coordinate axes and find coordinates of all joint where forces are acting.
- 2. Find virtual displacements.
- 3. Use POVW to find unknowns

Note: In POVW, we don't consider reaction at supports, because their work done is zero.

Example:



Find
$$P: Q = ?$$

Solution:

$$x_A = 2a\cos\theta$$
, $\partial x_A = -2a\sin\theta$ $\partial\theta$
 $x_B = +4a\cos\theta$, ∂x_B
 $= -4a\sin\theta$ $\partial\theta$

$$(VW)_P + (VW)_O$$

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$$P \cdot \partial x_{A} - Q \partial x_{B} = 0$$

$$P[-2a \sin \theta] \partial \theta - Q[-4a \sin \theta\theta]$$

$$= 0$$

$$-2P + 4Q = 0$$

$$\frac{P}{Q} = 2$$

Chapter 4: TRANSLATORY MOTION

Kinematics:

For a particle with $\vec{r} = x\hat{i} + y\hat{j} + z\hat{k}$

$$\vec{V} = \frac{\vec{d}r}{dt} \quad \vec{a} = \frac{d\overline{V}}{dt}$$



Acceleration (\vec{a}) :

• Uniform

$$v = u + at$$

$$S = ut + \frac{1}{2}at^2$$

$$V^2 = u^2 + 2as$$

Non-uniform

$$a = \frac{dV}{dt}$$

$$a = V \cdot \frac{dV}{ds}$$

Newton's Second Law (NSL):

For a particle:

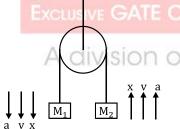
$$\sum \vec{F}_{\text{ext}} \neq 0 \text{ then } \vec{a} \neq 0$$

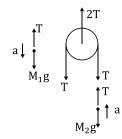
$$\vec{a} = \frac{\sum \vec{F}_{ext}}{m}$$
 NS

Dynamics:

Case A:

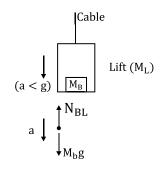
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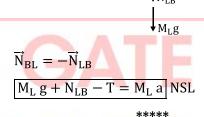
$$\begin{split} a &= \left(\frac{m_1 - m_2}{m_1 + m_2}\right) g \quad \begin{cases} m_1 g - T = m_1 a \rightarrow & \textcircled{1} \\ T - m_2 g = m_2 a \rightarrow & \textcircled{2} \end{cases} \\ T &= \left(\frac{2m_1 m_2}{m_1 + m_2}\right) g \end{split}$$

Case B:



$$M_B g - N_{BL} = M_B a$$
 NSL

For Lift



Chapter 5: CIRCULAR MOTION

Curvilinear Motion

$$\vec{r} = x\hat{i} + y\hat{j} + z\hat{k}$$

$$\vec{V} = \frac{d\vec{r}}{dt} = \frac{dx}{dt}\hat{i} + \frac{dy}{dt}\hat{j} + \frac{dz}{dt}\hat{k}$$

$$\overrightarrow{V} = V_x \hat{\imath} + V_y \hat{\jmath} + V_z \hat{k}$$

$$\vec{a} = a_x \hat{\imath} + a_y \hat{\jmath} + a_z \hat{k}$$

Projectile Motion:

$$Total\ time\ (T) = \frac{2U\sin\theta}{g}$$

$$\text{Max height (H}_{\text{max}}) = \frac{\text{U}^2 \sin^2 \theta}{\text{g}}$$

Horizontal Range
$$(R) = U_x . T$$

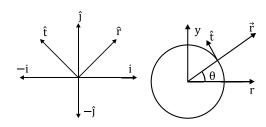
$$\boxed{R = \frac{U^2 \sin 2\theta}{g}} R_{max} \text{ at } \theta = 45^{\circ}$$



Equation of Trajectory:

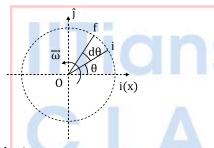
$$y = x \tan \theta - \frac{gx^2}{2 U^2 \cos^2 \theta}$$
or
$$y = x \tan \theta \left(1 - \frac{x}{R}\right)$$

Circulation Motion:



 $\vec{r} = \cos \theta \hat{i} + \sin \theta \hat{j}$

 $\hat{t} = \sin \theta (-\hat{i}) + \cos \theta (\hat{j})$



Angular velocity

$$\omega = \frac{d\theta}{dt} \rightarrow (rad/sec)_{SIVE} GATE COACHIN$$

Angular acceleration

Angular acceleration
$$\alpha = \frac{d\omega}{dt} \rightarrow rad/sec^{2}$$

$$\alpha = \frac{d\omega}{dt} \rightarrow rad/sec^{2}$$

$$\alpha = \frac{d\omega}{dt} \rightarrow rad/sec^{2}$$

$$\alpha = r\omega^{2}(-\hat{r}) + r\alpha(\hat{r})$$

Direction of ' ω ' and ' α ' \rightarrow Right hand thumb rule.

Angular acceleration:

Uniform

$$\omega = \omega_0 + \alpha t$$

$$d\theta = \omega_0 t + \frac{1}{2} \alpha t^2$$

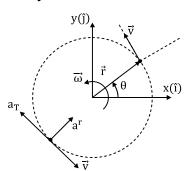
$$\omega^2 = \omega_0^2 + 2\alpha (d\theta)$$

Non-uniform

$$\alpha = \frac{d\theta}{dt}$$

$$\alpha = \omega \frac{d\omega}{d\theta}$$

Vector Analysis of Circular Motion:



$$\vec{r} = |r| \cdot \hat{r}$$

$$\vec{r} = r[\cos\theta \,\hat{\imath} + \sin\theta \,\hat{\jmath}]$$

$$\vec{V} = \frac{d\vec{r}}{dt} = r[-\sin\theta\hat{\imath} + \cos\theta\hat{\jmath}] \frac{d\theta}{dt}$$

$$\vec{V} = r\omega(\hat{t})$$

$$\vec{a} = \frac{d\vec{V}}{dt} = r \left(\omega \left(-\cos\theta \frac{d\theta}{dt} \ \hat{\imath} \right) \right)$$

$$-\sin\frac{\mathrm{d}\theta}{\mathrm{d}t}\hat{\jmath}\bigg)\bigg)(-\sin\theta\hat{\imath}$$

$$+\cos\theta\hat{j}\frac{d\omega}{dt}$$

$$\vec{a} = r\omega^2(-\cos\theta\,\hat{\imath} + (-\sin\theta)\hat{\jmath})$$

$$+ r\alpha(-\sin\theta\hat{i} + \cos\theta\hat{j})$$

$$\vec{a} = r\omega^2(-\hat{r}) + r\alpha(\hat{t})$$

$$\vec{a} = \vec{a}_r + \vec{a}_T$$

 $\vec{a}_r = radial/centripetal$ acceleration

 $\vec{a}_T = tangential acceleration$

$$a_r = r\omega^2 = \frac{V^2}{r}$$

For uniform circular motion

$$V = r \cdot \omega = constant$$

$$\omega = constant$$

$$\alpha = 0$$
, $\vec{a}_T = 0$

$$\vec{a} = \vec{a}_r$$



Chapter 6: FRICTION

Dry Friction/Coulomb Friction:

Static friction

Rest + Verge of motion

$$0 < f_s < f_{(s)_{max}}$$

$$(f_s)_{max} = \mu_s N$$

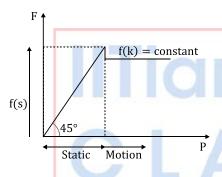
 μ_s = Coefficeint of static friction

N = Normal reaction

If applied force i.e:

$$P < (f_s)_{max}$$

then
$$(f_{(s)} = P)$$



Note:

 $\mu_s > \mu_k$

Then $f_s = \mu_k N$ Linear Momentum (\vec{P}) : $f_s = F_k$

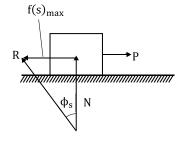
Kinetic friction

Motion

$$F_K = \mu_k N$$
 constant

Angle of Static Friction (ϕ_s):

Angle made by normal reaction with contact for de. Conservation of Linear Momentum \vec{P} :

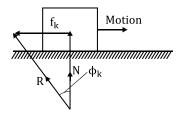


$$\tan \phi_s = \frac{(f_s)_{max}}{N}$$

$$\tan\varphi_s = \frac{\mu_s N}{N} = \mu_s$$

Angle of Kinetic Friction (ϕ_k):

During motion of body, the angle made by contact force with normal reaction is called as φ_k.



$$tan(\varphi_k) = \frac{f_k}{N} = \frac{\mu_k N}{N} = \mu_k$$

Note:

If μ_s and μ_k not given separately

1.
$$\mu_s = \mu_k = \mu$$

2.
$$0 \le f_s \le (f_s)_{max} = \mu N = f_k$$

3.
$$tan \phi = \mu \ (\phi = angle \ of \ friction)$$

Chapter 7: WORK & ENERGY

$$\vec{P} = m \cdot \vec{V}_{cm}$$

$$\frac{d\vec{P}}{dt} = m \cdot \frac{d\vec{V}_{cm}}{dt} \Rightarrow \frac{d\vec{P}}{dt} = \vec{m} \cdot \vec{a}_{cm} = \Sigma \vec{F}_{ext}$$

$$\sum \vec{F}_{\text{ext}} = \frac{d\vec{P}}{dt}$$

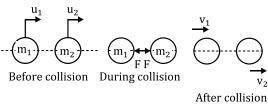
 \vec{P} = Constant

$$d\vec{P} = 0$$

Only when $\sum \vec{F}_{ext} = 0$ $P_x = constant; P_y = Constant$



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After collisio
$$[v_2 > v_1]$$

$$P_x = constant$$

$$m_1 u_1 + m_2 u_2 = m_1 v_1 + m_2 v_2$$

Collision:

1. Perfectly elastic collision $e = 1 (m_1 +$ m₂) system

$$(k\epsilon)_{initial\ of\ system} = (k\epsilon)_{Final\ of\ system}$$

$$\boxed{ \begin{aligned} \underline{m_1 u_1 + m_2 u_2 &= m_1 v_1 + m_2 v_2 \\ 1 &= \frac{1}{2} m_1 u_1 + \frac{1}{2} m_2 u_2 &= \frac{1}{2} m_1 v_1 + \frac{1}{2} m_2 v_2 \end{aligned}} \rightarrow \boxed{1}$$

$$(u_1 - u_2 = v_2 - v_1)$$

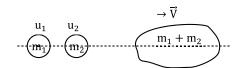
 $u_1 - u_2 = Velocity of approach$

$$v_2 - v_1 = Velocity of separation$$

$$\left(e = \frac{v_2 - v_1}{u_1 - u_2}\right) \text{ division of Pr}$$

e = coefficient of restitution

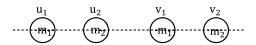
2. Perfectly Inelastic (Plastic) collision (e = 0)



$$m_1u_1 + m_2u_2 = (m_1 + m_2)v$$

 $(k\varepsilon)_{loss} = (k\varepsilon)_{initial} - (k\varepsilon)_{final}$

3. Partially Elastic Collision: (0 < e < 1)

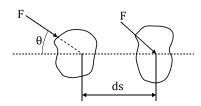


No complete region in size ⇒ Same energy loss due to deformation.

kε ≠ conserved

$$m_1u_1 + m_2u_2 = m_1v_1 + m_2v_2$$

Work done:



$$WD = \vec{F} \cdot \vec{d}s = F ds \cos \theta$$

$$(WD)_{spring} = \int Fs \, dx = -\frac{1}{2} kx^2$$

Work Energy Theorem:

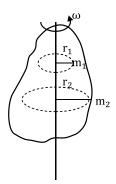
Work done by all the forces acting on a particle = change in kinetic energy

$$W_{\text{net}} = (k\epsilon)_{\text{final}} - (k\epsilon)_{\text{initial}}$$

If $(work done)_{non conservative} = 0$

Then mechanical energy = constant

Rotation of Rigid Bodies:



Mass moment of inertia

$$I = m_1 r_1^2 + m_2 r_2^2 + m_3 r_3^2 + \cdots$$

$$I = \sum m_i r_i^2$$

Let $\sum M_i = m = Total mass$



$$I = mk^2$$

k = radius of gyration

Ring/Hollow Cylinder:

$$I = mR^2$$

Rod:

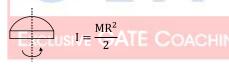


$$I_{cm} = \frac{mL^2}{12}$$

Solid Sphere



Disc/Hollow Cylinder



Hollow sphere

$$I = \frac{2}{3} mR^2$$

Rod about end



$$J = \frac{mL^2}{3}$$

Dynamics of Rigid Body Rotation:

If
$$\sum \overrightarrow{T}_{net} = 0$$
 then $\overrightarrow{\alpha} = 0$

If
$$\sum \overrightarrow{T} \neq 0$$
 then $\overrightarrow{\alpha} \neq 0$

$$\sum \vec{T}_{net} = I \cdot \vec{\alpha}$$

$$\Sigma \vec{T}_{cm} = I_{cm} \cdot \alpha$$

$$\Sigma \vec{T}_{Axis} = I_{Axis} \cdot \alpha$$

Angular Momentum (\vec{L}) (Moment of linear momentum)

$$\vec{L} = \vec{r} \times \vec{P}$$

$$\Sigma \vec{T} = \frac{dL}{dt}$$

Conservation of Angular Momentum:

$$\vec{L} = \text{Constant}, dL = 0, \text{ when } \Sigma \vec{T} = 0$$

Eg:
$$I_1\omega_1 = I_2\omega_2$$

Rotational Kinetic Energy

$$k\epsilon = \sum_{i=1}^{n} \frac{1}{2} m_i V_i^2 = \sum_{i=1}^{n} \frac{1}{2} m_i r_i^2 w_i^2$$

$$k\epsilon = \frac{1}{2}I \cdot \omega^2$$

BY 111/11Se GRADUATES Word done:

$$(wD)_{T} = T \cdot d\theta$$

$$+ve$$
 $-ve$ θ

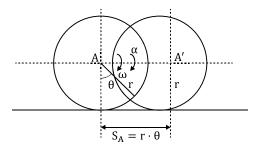
Power (P) =
$$T \cdot \frac{d\theta}{dt} = T \cdot w$$

= $\frac{2\pi NT}{60} (N \rightarrow rpm)$



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General Motion = Rotation + Translation



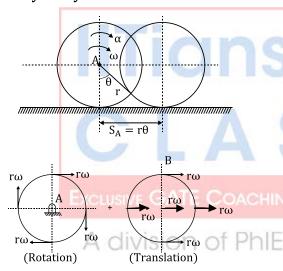
Conditions:

If $S_A = r\theta \rightarrow Pure rolling (V = r\omega \ a = r\alpha)$

If $S_A > r\theta \rightarrow Skidding$

If $S_A > r\theta \rightarrow Slipping$

Velocity Analysis:



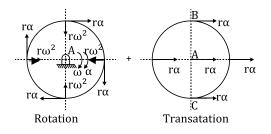
$$\overrightarrow{V}_T = \overrightarrow{V}_{Translation} + \overrightarrow{V}_{rotation}$$

$$\vec{V}_A = rw\hat{\imath} + 0 = r\omega$$

$$\vec{V}_B = r\omega i + r\omega \hat{i} = 2r\omega \hat{i}$$

$$V_c = r\omega \hat{i} - r\omega \hat{i} = 0$$
 (Pure rolling)

Acceleration Analysis:



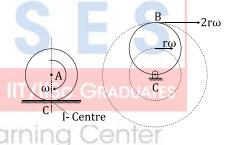
$$\begin{aligned} \vec{a}_T &= \vec{a}_{Trass} + \vec{a}_{Rot} \\ a_B &= r\alpha \hat{i} + r\alpha \hat{i} - r\omega^2 \hat{j} = 2r\alpha \hat{i} - r\omega^2 \hat{j} \\ a_C &= r\alpha \hat{i} - r\alpha \hat{i} + r^2\alpha \hat{j} \\ \\ \boxed{\vec{a}_C \neq 0} \end{aligned}$$

Note:

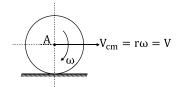
- In pure rolling static friction will be there on the roller, because contact point has zero velocity.
- 2. Energy of a roller rolling on rough surface remains conserved because the work done by static friction = 0.

I-Centre (Instantaneous Centre)

Point about which a body is in general motion can be assumed in pure rotation to find velocity only.



Kinetic Energy in Rolling:



Body is rolling due to applied torque (T)

$$(k\varepsilon)_{\text{Rolling}} = \frac{1}{2} \text{mV}^2 + \frac{1}{2} I_A \omega^2$$

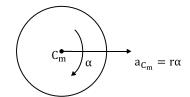
$$= \frac{1}{2} \text{mr}^2 \omega^2 + \frac{1}{2} I_A \omega^2$$

$$= \frac{\omega^2}{2} [I_A + \text{mr}^2]$$

$$(K\varepsilon)_{\text{rolling}} = \frac{1}{2} I_C \cdot \omega^2$$



Dynamics:



$$\sum F_{\text{net}} = ma_{\text{cm}} \text{ (NSL)}$$

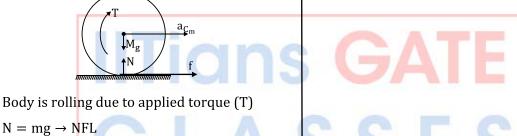
$$\sum F_{net} = m \cdot r\alpha \rightarrow 1$$

$${\textstyle \sum} T_{C_m} = I_{C_m} \times \alpha$$

$$\sum T_{Axis} = I_{Axis} \times \alpha$$

Friction in Rolling:

Case 1:



$$N = mg \rightarrow NFL$$

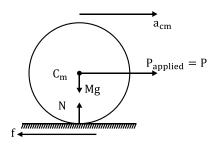
$$F = m a_{cm} \rightarrow NSL$$

$$F = m r \alpha \qquad (T_{app} = T)$$

$$\Sigma T_{cm} = I_{cm}$$
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$$(T_{app} - F(r)) = I_{C_m}\alpha_{ivision}$$
 of PhIE Learning Center

Case 2:



In this case friction will roll the body

$$P_{app} - f(r) = m \cdot a_{cm}$$

$$a_{cm} = r\alpha$$

$$F(r) = I_{cm}\alpha$$

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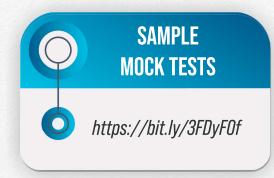
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